

## In the Claims

1. (currently amended) A method for modeling ~~an object~~ a moving object composed of one or more components, comprising:

inputting data for each component of the object, the data including coordinates expressed in Euclidean space for a plurality of points  $\mathbf{x}$  of each component;

encoding, for each component, each point  $\mathbf{x}$  as a null vector  $x$  in a homogeneous space by  $x = (\mathbf{x} + \frac{1}{2}\mathbf{x}^2e + e_*)E = \mathbf{x}E - \frac{1}{2}\mathbf{x}^2e + e_*$ , where  $e$  and  $e_*$  are null vectors of with unit bivector  $E = e \wedge e$ ; ~~and~~

associating a plurality of general homogeneous operators with each ~~data~~ construct component to generate a model of the object; and

determining a motion of the object by a time dependent displacement versor  $D=D(t)$  satisfying a differential equation  $\dot{D} = \frac{1}{2}VD$ , with “screw velocity”  $V$  given by  $V = -I\omega + e\mathbf{v}$ , where  $\omega$  is a velocity and  $\mathbf{v}$  is a rotational translational velocity of the object, wherein the object is a rigid body.

2. (original) The method of claim 1 further comprising:

supplying run-time parameters for the plurality of operators; and  
applying the plurality of general homogeneous operators to each encoded point  $\mathbf{x}$  of each associated component to manipulate the model of the object.

3. (previously amended) The method of claim 1 further comprising:

measuring a scalar distance  $\mathbf{d}_{ab}$  between two component points  $\mathbf{a}$  and  $\mathbf{b}$  encoded as homogeneous points  $a$  and  $b$  by  $\mathbf{d}_{ab}^2 = (a - b)^2 = -2a \bullet b$ .

4. (previously amended) The method of claim 1 wherein a line through component points **a** and **b** encoded as homogeneous points  $a$  and  $b$  is modeled by  $e \wedge a \wedge b$ , and a length  $l_{ab}$  of a line segment connecting component points **a** and **b** is generated by:

$$(l_{ab})^2 = (e \wedge a \wedge b)^2 = (a - b)^2.$$

5. (previously amended) The method of claim 1 wherein a plane through component points **a**, **b**, and **c** encoded as homogeneous points  $a$ ,  $b$ , and  $c$  is modeled by  $e \wedge a \wedge b \wedge c$ , and an area  $A_{abc}$  is generated by  $(A_{abc})^2 = \frac{1}{4} (e \wedge a \wedge b \wedge c)^2$ .

6. (previously amended) The method of claim 1 wherein a sphere  $s$  with radius  $r$  centered at a component point **c** encoded as homogeneous point  $c$  is encoded as a vector  $s = c + \frac{1}{2} r^2 e$ .

7. (previously amended) The method of claim 1 wherein a sphere  $s$  determined by four component points **a**, **b**, **c**, **d** encoded as homogeneous points  $a, b, c, d$  is generated by  $s = (a \wedge b \wedge c)(a \wedge b \wedge c \wedge e)^{-1}$ .

8. (currently amended) The method of claim 8 wherein a plane through component points  $a, b, c$  is encoded as a vector  $p = I(a \wedge b \wedge c \wedge e) |a \wedge b \wedge c \wedge e|^{-1}$ , where  $I$  is a unit pseudoscalar.

9. (previously amended) The method of claim 8 wherein a distance between a component homogeneous point **a** and a component plane **p** is generated by an inner product  $a \bullet p$ .

10. (previously amended) The method of claim 6 wherein a distances between a homogeneous component point  $\mathbf{a}$  and a component sphere  $\mathbf{s}$  is generated by an inner product  $\mathbf{a} \bullet \mathbf{s}$ .

11. (previously amended) The method of claim 6 wherein a distance between two component spheres  $s_1 = c_1 + \frac{1}{2}r_1^2 e$  and  $s_2 = c_2 + \frac{1}{2}r_2^2 e$  is generated by  $s_1 \bullet s_2 = c_1 \bullet c_2 + \frac{1}{2}(r_1^2 + r_2^2) = \frac{1}{2}[(r_1^2 + r_2^2) - (c_1 - c_2)^2]$ .

12. (cancelled)

13. (previously amended) The method of claim 12 wherein dynamics of the rigid body are determined by a differential equation  $\dot{P} = W$ , where  $P = -I\mathbf{L} + e_*\mathbf{p}$ , and  $W = -I\mathbf{T} + e_*\mathbf{F}$ , where  $\mathbf{L}$  is an angular momentum and  $\mathbf{p}$  is a translational momentum of the rigid body, while  $\mathbf{T}$  is a net torque and  $\mathbf{F}$  is a net force on the rigid body.

14. (previously amended) The method of claim 12 wherein the rigid body includes  $n$  linked rigid components, and a motion of the rigid body is modeled by  $n$  time dependent displacement versors  $D_1, D_2, \dots, D_n$ , with a motion of a  $k^{\text{th}}$  linked rigid component determined by a versor product  $D_1 D_2 \dots D_k$ .

15. (previously amended) The method of claim 1 wherein the objects is a robot composed of a plurality of rigid bodies connected at joints.